

Analog

Oct 18

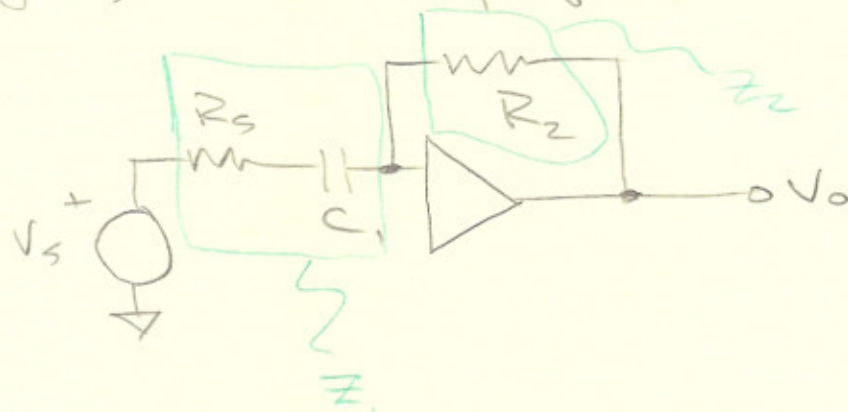
1.

Assignment #4. 5.15, 5.17, 5.20, 5.30  
Due Tues Oct 30.

DP 5.22

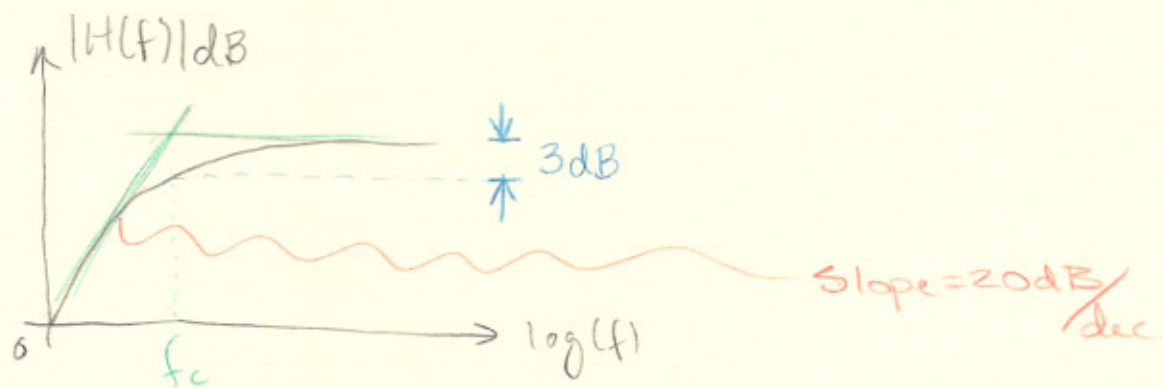
Design for cut off freq 100 kHz

All



$$z_1 = R_s + \frac{1}{j\omega C_1} \quad z_2 = R_2$$

$$H(f) = \frac{V_o}{V_s} = \frac{-R_2}{R_s + \frac{1}{j\omega C_1}} = \frac{-R_2 j\omega C_1}{1 + j\omega C_1 R_s}$$



$$f \rightarrow \infty \Rightarrow |H(f)| = \frac{R_2}{R_s}$$

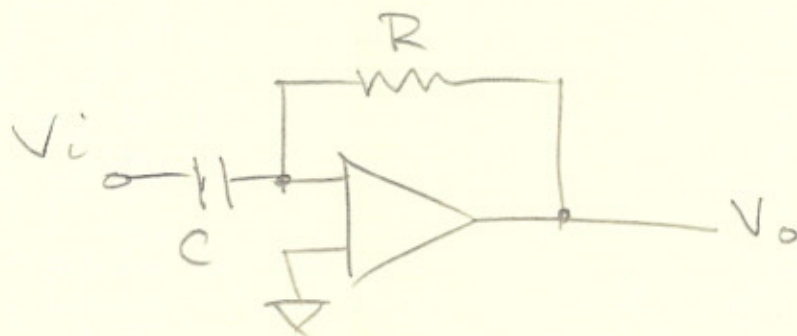
$$f \rightarrow 0 \Rightarrow |H(f)| = 0$$

$$\omega_c R_5 C_1 = 1 \Rightarrow f_c = \frac{1}{2\pi R_5 C_1}$$

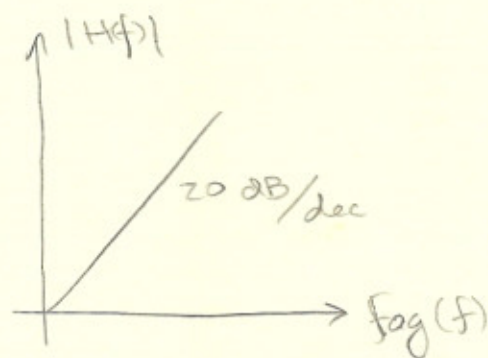
note:

$$20 \log\left(\frac{1}{\sqrt{2}}\right) = -3 \text{ dB}$$

Ideal Differential Ckt.



$$\frac{V_o}{V_i} = -RC \frac{dV_i}{dt}$$



EX: Continued from last example.

$$100 \text{ kHz} = \frac{1}{2\pi (1 \text{ k}\Omega) C_1}$$

$$C_1 \sim 1.6 \text{ nF}$$

Take  $R_s = R_z$  we have unity gain

b//  $R_s \rightarrow 800 \Omega$

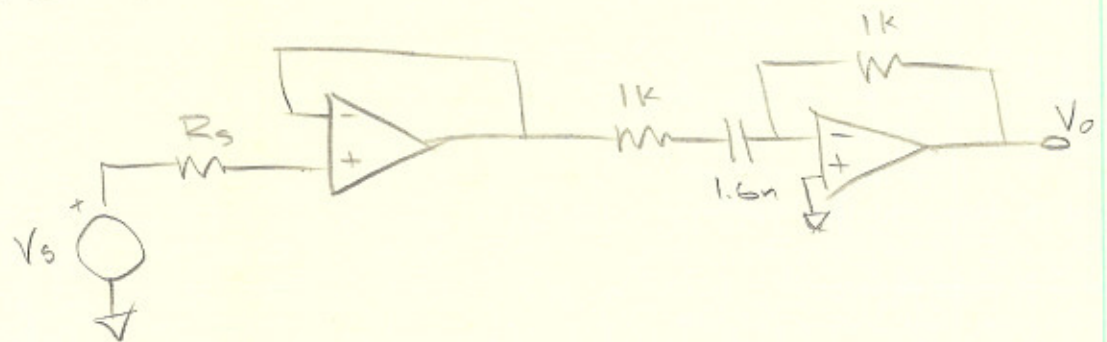
$f_c = 124 \text{ kHz}$

note: Gain also increase

c// Make  $f_c$  independent of  $R_s$ .

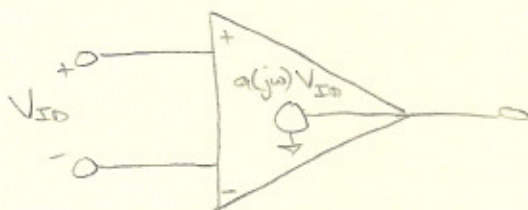
We can put a resistor in series or parallel so that  $R_s$  is neglected in  $f_c$  calculation. However here we are attenuating the input signal, hence increasing the signal to noise ratio

The best solution however would be to add a voltage follower before the circuit,

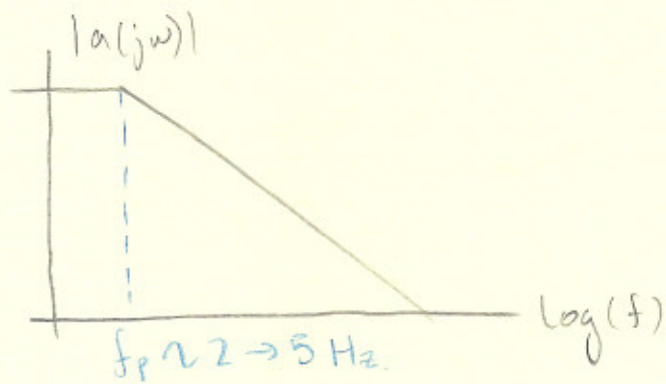


### Non Ideal O.A. Characteristics

- \* Offset Voltage
- \* Finite gain
- \* Finite bandwidth (most important)



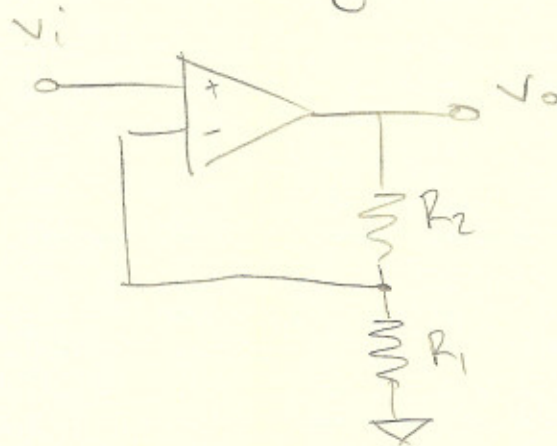




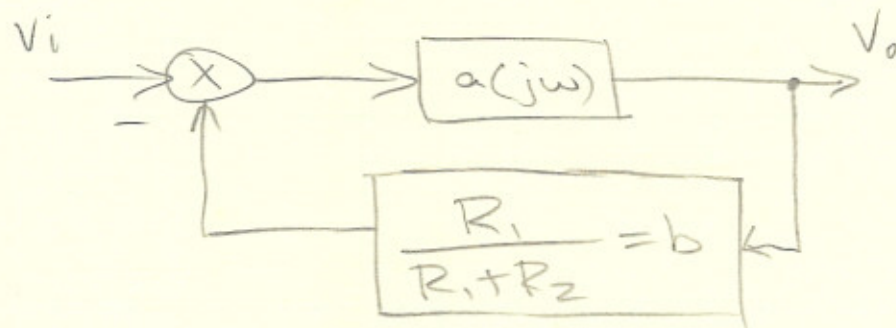
$$a(j\omega) = \frac{a_0}{1 + j\frac{\omega}{\omega_p}} \quad ; \quad \omega_p = 2\pi f_p.$$

EX

Non-inverting amp.



$$\begin{aligned} \frac{V_o}{V_i} &= \frac{\frac{a_0}{1 + j\omega/\omega_p}}{1 + \frac{a}{1 + j\omega/\omega_p} \frac{R_1}{R_1 + R_2}} \\ &= \frac{a_0}{1 + j\frac{\omega}{\omega_p} + a_0 \frac{R_1}{R_1 + R_2}} \end{aligned}$$



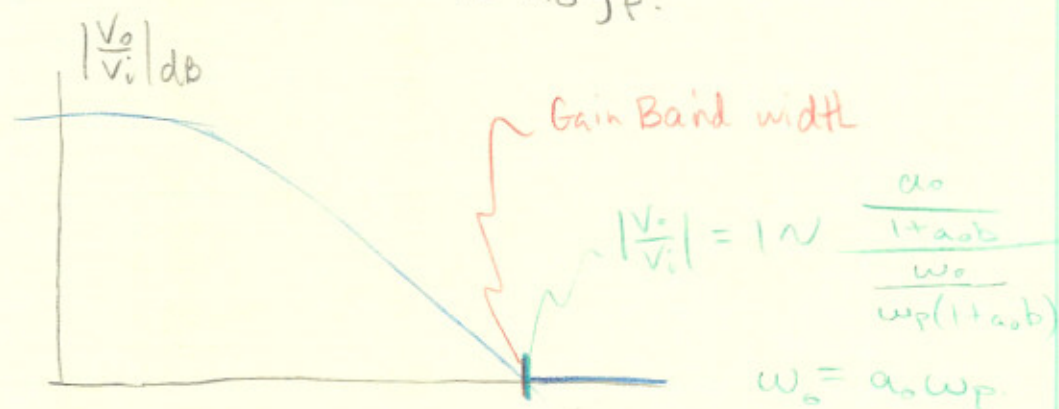
$$\frac{V_o}{V_i} = \frac{a_o}{1 + a_o b} \cdot \frac{1}{1 + j \frac{\omega}{\omega_p}(a_o b + 1)}$$

$$\omega \rightarrow 0 \Rightarrow \frac{V_o}{V_i} = \frac{a_o}{1 + a_o b}$$

$$\text{if } a \rightarrow \infty \Rightarrow \frac{V_o}{V_i} = \frac{1}{b}$$

$$\begin{aligned} \text{Pole freq, } f_c &= \frac{\omega_p(a_o b + 1)}{2\pi} \\ &= f_p(a_o b + 1) \end{aligned}$$

$$\begin{aligned} \text{Product (DC gain)} \times (f_c) &= \frac{a_o}{1 + a_o b} \cdot f_p(a_o b + 1) \\ &= a_o f_p. \end{aligned}$$



## Inverting Amplifier

$$\frac{V_o}{V_i} = \frac{-R_z a_o}{R_i(1+a_o) + R_z} \cdot \frac{1}{1 + j \frac{R_i + R_z}{R_i(1+a_o) + R_z} \frac{\omega}{\omega_p}}$$

for high freq, imaginary part  $\gg 1$

$$\left| \frac{V_o}{V_i} \right| = 1 \approx \frac{R_z a_o}{R_i(1+a_o) + R_z} \Rightarrow \text{some shit... check the text.}$$

$$\frac{R_i + R_z}{R_i(1+a_o)} \approx \frac{\omega_o}{\omega_p}$$